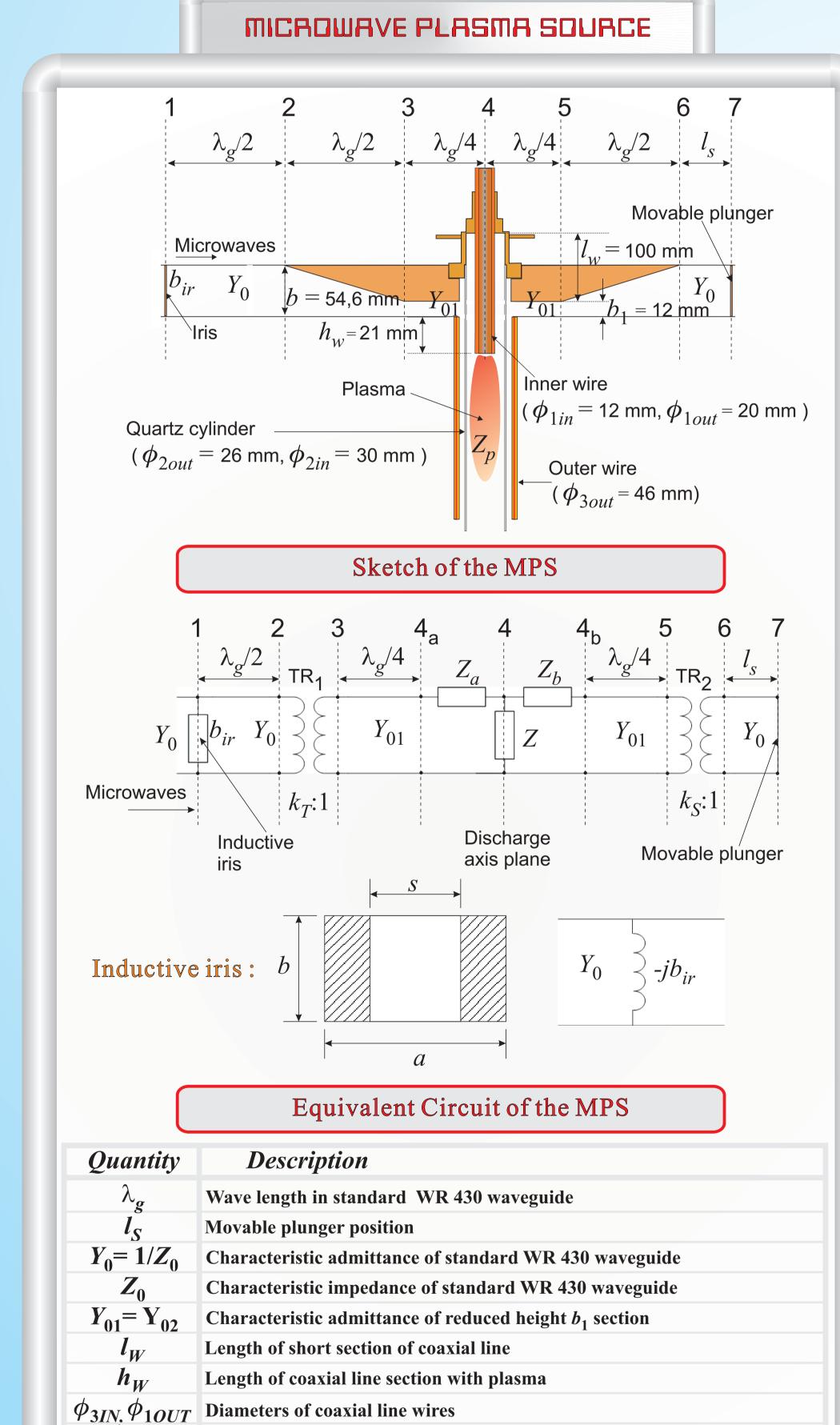


INTRODUCTION

We present equivalent circuit of existing waveguide-based coaxial-type microwave plasma source (MPS) which was used to hydrogen production via methane reforming. This MPS is operating at frequency of 2.45 GHz, in different gases at atmospheric pressure. The equivalent circuit cannot describe all electrical properties of the real MPS accurately due to some structural elements, which electrical lumped equivalents are difficult to find or are unknown. We used Comsol Multiphysics software to numerical investigate the unknown lumped impedance of some structural elements. The equivalent circuit includes formula which allows to calculate tuning characteristics which are one of essential indicator of power transfer from the feeding line to the MPS. The MPS is terminated with movable plunger which plays the role of the tuning element. Despite of the fact that the equivalent circuit describes specific MPS, it can be helpful to examine theoretically any similar waveguide-based coaxial-type MPSs.



FORMULAS

 $b_{ir} = \frac{B_{ir}}{Y_0} = -\frac{\lambda_g}{a} ctg^2(\frac{\pi s}{2a})$

 $k_T = \frac{Y_0}{Y_{01}}$ $k_S = \frac{Y_{01}}{Y_0} = k_T^{-1}$

 $b_{S} = \frac{B_{S}}{Y_{0}} = ctg(\frac{2\pi}{\lambda_{a}} \cdot l_{S}) = t_{S}^{-1}$

 $Y = (jX_W + Z_p^t + jX)^{-1}$

 $X_W = Z_{0W} \cdot tg(\frac{2\pi}{\lambda} l_W)$

 $Z_{0W} = 60 \ln(\frac{\phi_{3IN}}{\phi_{1OUT}})$

Normalized susceptance of iris:

Transformation factors:

Normalized movable plunger susceptance in output plane:

Admittance in discharge axis:

Reactance of short coaxial line section:

Characteristic impedance of coaxial line:

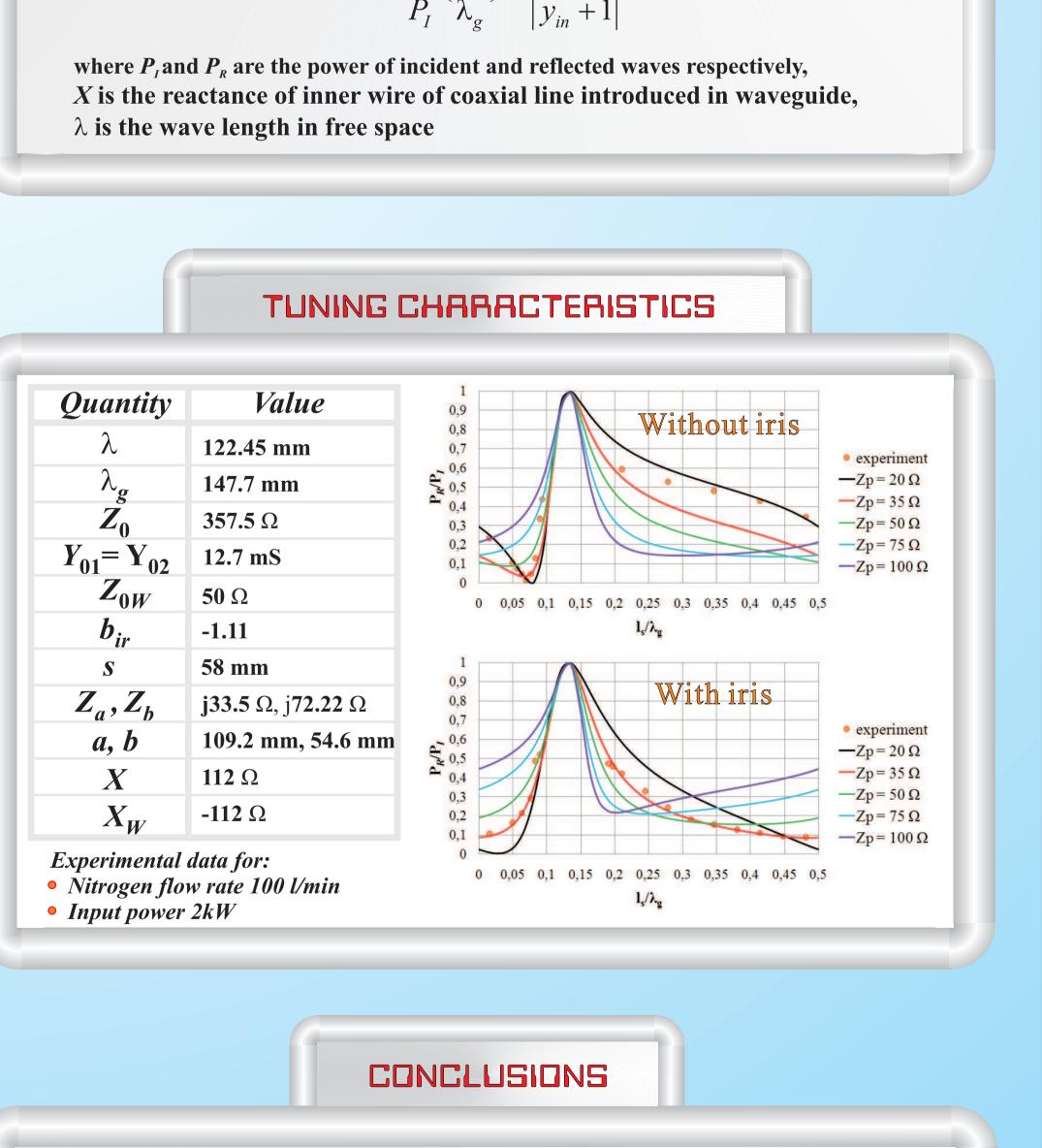
Plasma impedance transformed via coaxial line of h_w lenght: $Z_p^t(h_w) = Z_{0W} \frac{Z_p + jZ_{0W}tg(\frac{2\pi}{\lambda}h_w)}{Z_{0W} + jZ_ptg(\frac{2\pi}{\lambda}h_w)}$

Normalized input admittance:

 $y_{in} = \frac{Y_1}{Y_0} = k_S \frac{Z^{-1} \cdot (Z_b Y_{01} - jt_S^{-1}) + Y_{01}}{Z_a [Y(Z_b Y_{01}^2 - jk_S Y_0 t_S^{-1}) + Y_{01}^2] - jk_S Y_0 t_S^{-1}} + jb_{ir}$

Tuning characteristic:

 $\frac{P_R}{P_I}(\frac{l_S}{\lambda_g}) = \left|\frac{y_{in}-1}{y_{in}+1}\right|^2$



Z_p	Plasma impedance
b _{ir}	Normalized susceptance of inductive iris
S	Width of the inductive iris
Z_a, Z_b	Impedances representing discontinuity (holes) in reduced height waveguide
k_T, k_S	Transformation factors of the input and output transformer respectively
<i>a</i> , <i>b</i>	Standard WR 430 waveguide width and height respectively
Z	Impedance in discharge axis

- The calculated results and results achieved in experiment are very similar for assumed plasma impedance $Z_p = 35 \Omega$, and reactance $X = -X_W$
- The power reflection coefficient P_R/P_I of the MPS with iris is small for wide range of normalized movable plunger position
- The presented equivalent circuit of the MPS can be helpful to improve any similar MPSs.

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